Using a 1.2 GHz bandwidth reflective semiconductor optical amplifier with seeding light by 64-quadrature amplitude modulation orthogonal frequency division multiplexing modulation to achieve a 10-gbits/s upstream rate in long-reach passive optical network access

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1 Introduction

In order to deliver the future broadband multi-services economically (such as data, voice, CATV, IPTV, 3D-TV, etc.), network operators need to reduce costs to sustain profit margins. One possible method is to simplify the fiber network architecture, which would lead to the reduction of the number of equipment interfaces and network devices. Hence, a long-reach (LR) access network has been proposed to solve this issue.1,2 The LR passive optical network (PON) can combine metro and access networks into a single system that has the benefit of high capacity and a high split ratio, and the transmission can reach 40 to 100 km.3

Moreover, hybrid wavelength division multiplexing—time division multiplexing (WDM-TDM) PON has been considered as a potential solution for next-generation PON. Due to the bandwidth sharing of the TDM-PON, the hybrid WDM-TDM PON would provide a relative lower per-subscriber cost than pure WDM-PON by dividing a single wavelength to multiple subscribers while still maintaining a relatively high per-subscriber bandwidth.4 In the WDM PON and hybrid WDM-TDM PON, using a centralized light source in a central office (CO) has been proposed to reduce costs by removing the laser sources from the subscribers in PON, which can in turn reduce the inventory cost and simply the wavelength management.5 Recently, using optical orthogonal frequency division multiplexing (OFDM) modulation in carrier-distributed PONs to effectively enhance the transmission data rate and reduce costs has raised research interests.6,7 In these carrier-distributed PONs, a reflective semiconductor optical amplifier (RSOA) is usually used in each optical network unit (ONU) with upstream data rates of 1.25- or 2.5 g bits/s OOK remodulation depending on the injection powers from the CO.5,8 and the current commercially available RSOA can only achieve 2.5 g bits/s OOK remodulation even under a high optical injection power.

We propose and demonstrate 10 g bits/s upstream traffic in a carrier-distributed LR-PON using a 1.2 GHz bandwidth RSOA-based ONU and 64-QAM OFDM modulation. In the carrier-distributed PON, a continuous wave (CW) optical signal is launched into the RSOA from the CO. Here, 20, 50, and 75 km-long single-mode fiber (SMF) transmissions are investigated in the proposed PON to determine the relationship between transmission length and the signal-to-noise ratio (SNR). Moreover, we also discuss and analyze the upstream traffic performance when different CW injection levels are launched into RSOA.
2 Experiment

Figure 1 shows the proposed carrier-distributed hybrid WDM-TDM PON using RSOA-based ONU for 10 g bits/s optical OFDM-QAM modulation upstream traffic. In the CO, we used two wavelength bands for the downstream data and CW signals distributed to each ONU via a 1 × N WDM multiplexer and a 1 × M optical splitter. The downstream data and CW wavelengths were divided by a 1 × 2 WDM coupler on each ONU, as shown in Fig. 1. Here, the CW wavelength was launched into the RSOA to generate the upstream optical OFDM-QAM signal. In the practical PON system, we used two fibers to avoid the Rayleigh backscattering noise when the colorless upstream wavelength was employed.

Figure 2 shows the experimental setup for evaluating the proposed RSOA-based ONU to achieve the 10 g bits/s 64-QAM OFDM upstream data rate in the carrier-distributed PON. The RSOA (produced by CIP) had a 1.2 GHz bandwidth when operated at a 50 mA bias current. A CW wavelength of 1550.0 nm was distributed from the CO through the upper SMF with different lengths of 20, 50, and 75 km and was then injected into the RSOA via an optical circulator (OC), as illustrated in Fig. 2. An erbium-doped fiber amplifier (EDFA) (with a gain of 23 dB and noise figure of 5 dB) and optical variable attenuator were utilized to adjust the different CW injection power levels launching into the RSOA. Furthermore, the relaxation oscillation frequency of RSOA could be increased by optical injection; hence, a higher optical power increased the modulation speed of the RSOA. Here, Fig. 3 presents the output powers of the RSOA versus different CW injection power levels of −15 to 5 dBm, and the corresponding output powers of RSOA are also measured among 0.3 and 5.6 dBm.

In our experiment, the baseband electrical OFDM upstream signal was generated by an arbitrary waveform generator (AWG) utilizing the Matlab® program. The signal processing of the OFDM transmitter consisted of a serial-to-parallel conversion, QAM symbol encoding, inverse fast Fourier transform (FFT), cyclic prefix (CP) insertion, and digital-to-analog conversion (DAC). A 12 g sample/s sampling rate and an 8 bit DAC resolution were set by the AWG, and a CP of 1/64 was used. Thus, 72 subcarriers of the 64-QAM format occupied nearly 1.66 GHz bandwidth of 0.26 to 1.92 GHz, with an FFT size of 512. Here, a yield of approximately 22 MHz subcarrier spacing and approximately 10 g bits/s total data rate were observed. Thus, the produced electrical 64-QAM OFDM signal could be applied on RSOA via a bias tee. The upstream signal was then propagated via the OC and lower SMF to the CO, as shown in Fig. 2. The upstream signal was direct detected via a 2.5 GHz PIN receiver at the CO without using a pre-amplifier, and the received OFDM signal was captured by a real-time 50 GHz sampling oscilloscope for signal demodulation. To demodulate the vector signal, the off-line DSP program was employed, and the demodulation process contained the synchronization, FFT, one-tap equalization, and QAM symbol decoding. Therefore, the bit error rate (BER) was calculated according to the observed SNR.

Figure 4 shows the measured SNR of each OFDM subcarrier in the frequency bandwidth of 0.26 to 1.92 GHz with different SMF transmissions at back-to-back (B2B), 20 km, 50 km, and 75 km, respectively, without dispersion compensation under different CW injection power levels of −3 to 0 dBm launching into RSOA. In this measurement, the optical received power was fixed at −6 dBm and the CW injection power of −2 dBm was launched into RSOA. The entire measured subcarriers achieved the forward error correction (FEC) threshold [BER = 3.8 × 10−3 (SNR = 21.2 dB) and redundancy ratio of 7%] at B2B, 20 km, and 50 km, respectively, as shown in Fig. 4. However, when the transmission fiber length was 75 km, the measured SNR for some high frequency subcarriers could not achieve the FEC threshold due to fiber chromatic dispersion. As also shown in Fig. 4, when we decreased the CW injection power level gradually, the subcarriers at high frequency also experienced a SNR penalty simultaneously owing to the reduction in relaxation oscillation frequency of the RSOA. Due to the power fading and fiber dispersion effects after a 100 km fiber transmission via the 64-QAM OFDM modulation, the required SNR of each subcarrier was worse in the measurement.
Here, even when we increased the injected power to 4 dBm, the upstream signal was unable to transmit over 100 km in length.

We also investigated the BER measurement in different CW injection levels and transmission lengths. Figure 5 shows the BER performance of RSOA-based upstream signal at the B2B, 20-, 50-, and 75 km SMF transmissions, respectively, in the CW injection power levels of 4 to −10 dBm, when the received power is fixed at −6 dBm. The inserts of Fig. 5 are the corresponding constellation diagrams measured at the FEC threshold. To achieve the FEC threshold level at the B2B, 20-, 50-, and 75 km transmissions, the minimum CW injection powers had to be larger than −9, −8, −6, and −1 dBm, respectively, as illustrated in Fig. 5.

Finally, according to the measured results of Fig. 5, we set the CW injection power of −1 dBm launching into RSOA for the upstream transmission. Figure 6 presents the BER performances of RSOA-based 10 g bits/s 64-QAM OFDM upstream signal at the B2B, 20-, 50-, and 75 km SMF propagations, respectively. The inserts of Fig. 6 are corresponding constellation diagrams. In Fig. 6, we can observe the received powers at −12.6, −12.2, −10.8, and −7.4 dBm at B2B, 20-, 50-, and 75 km fiber transmissions, respectively, at the FEC threshold level. The measured power penalty of 5.2 dB was observed after a 75 km SMF transmission at the BER of $3.8 \times 10^{-3}$. In a LR-PON system, we added the EDFA, with a 23 dBm saturated power and approximate 5 dB noise figure, in the exchange node to enhance the injection power of seeding light for maintaining a −1 dBm seeding power.

3 Conclusion

We have proposed and demonstrated 10 g bits/s upstream traffic in a carrier-distributed LR-PON using a commercially available 1.2 GHz bandwidth RSOA-based ONU and a 64-QAM optical OFDM modulation. In this carrier-distributed PON, a CW optical signal was launched into the RSOA from the CO, and 20-, 50-, and 75 km SMF transmissions were evaluated. In the measurement, when the CW injection power was −1 dBm, the SMF transmission length of the RSOA-based upstream could achieve 20, 50, and 75 km simultaneously at the FEC threshold level (BER = $3.8 \times 10^{-3}$). The generated penalties of 0.4, 1.8, and 5.2 dB were also measured after 20-, 50-, and 75-km fiber transmissions, respectively, in the proposed RSOA-based ONU LR-PON system.

References


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